



Mechanical and  
Aerospace  
Engineering



# NSTX-U feedforward shape control and neural net dynamics modeling

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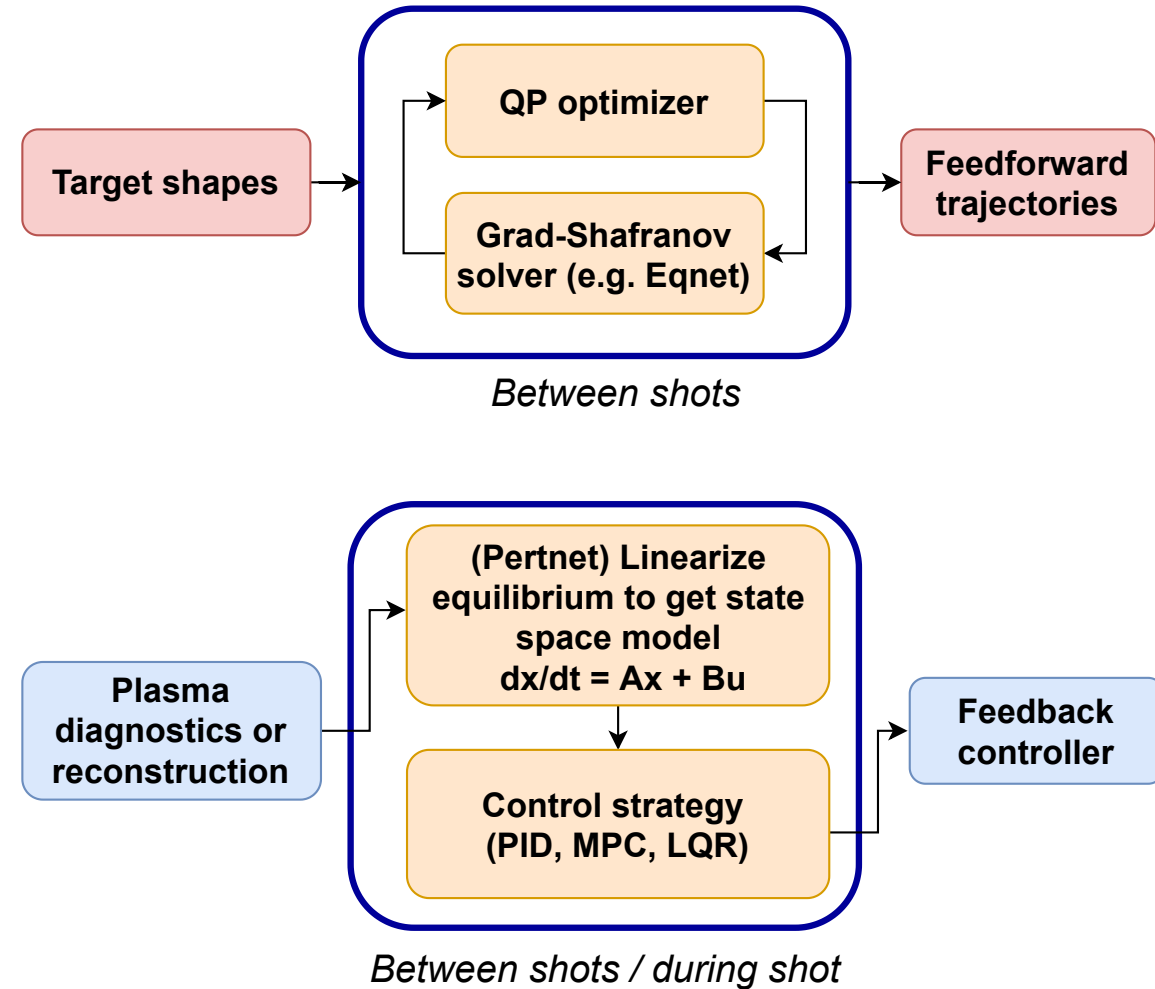
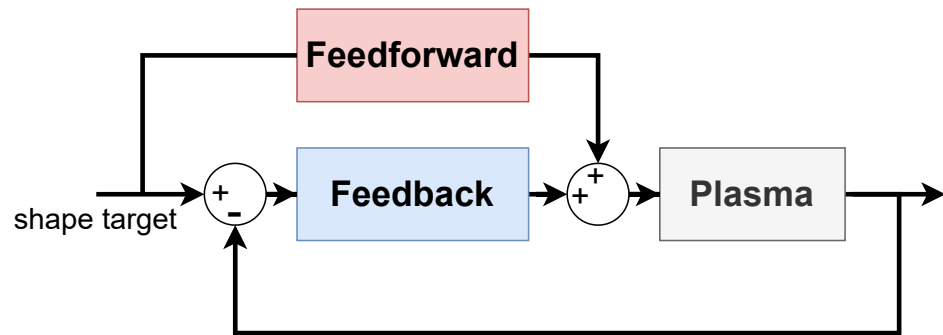
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# Executive summary (1 of 2)

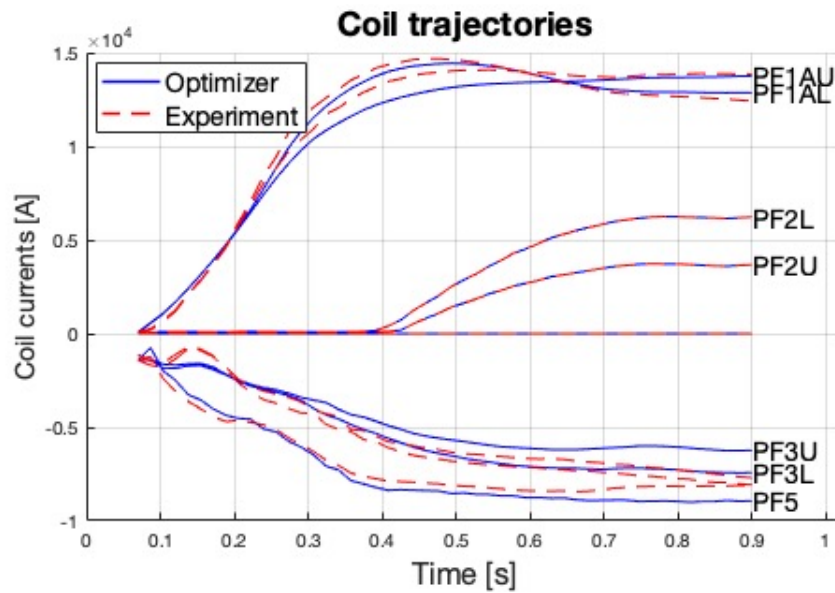
- Upgrading the NSTX-U shape controller to use **feedback and feedforward**, due to performance issues last campaign.
- Designed optimizer and neural nets that will enable fast feedforward and feedback control design.



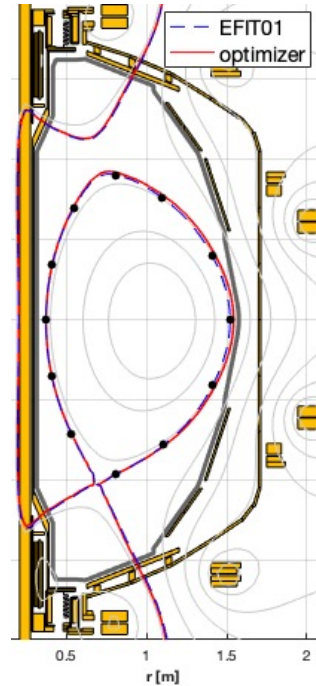
# Executive summary (2 of 2)

Shape optimizer uses input shapes to estimate coil current trajectories.

- successfully recreates old shots.
- will improve control, shot planning, and constraint avoidance.



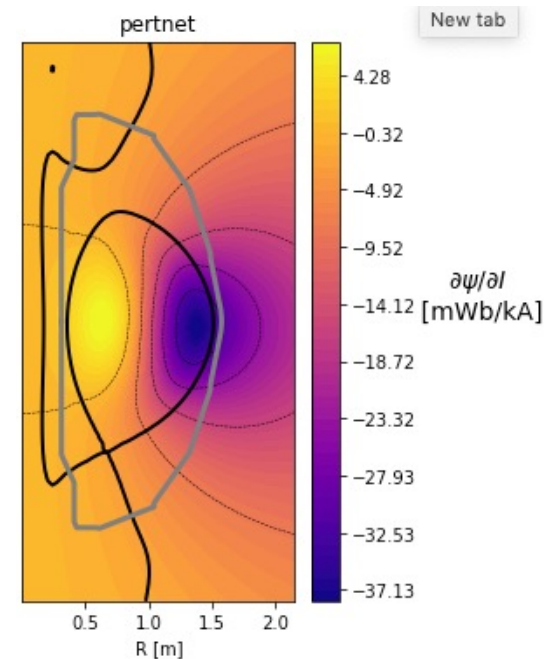
Optimizer successfully recreates coil current trajectories.



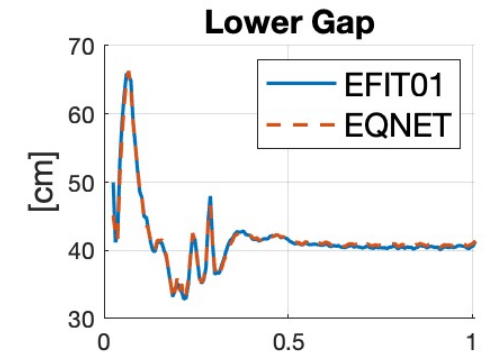
Optimizer successfully recreates equilibrium shapes.

Developed (complementary) shape control neural nets, for fast calculation and simulation.

- Eqnet: predicts equilibrium/shape parameters.
- Pertnet: predicts dynamical model



Neural net prediction of plasma response (dynamics model)

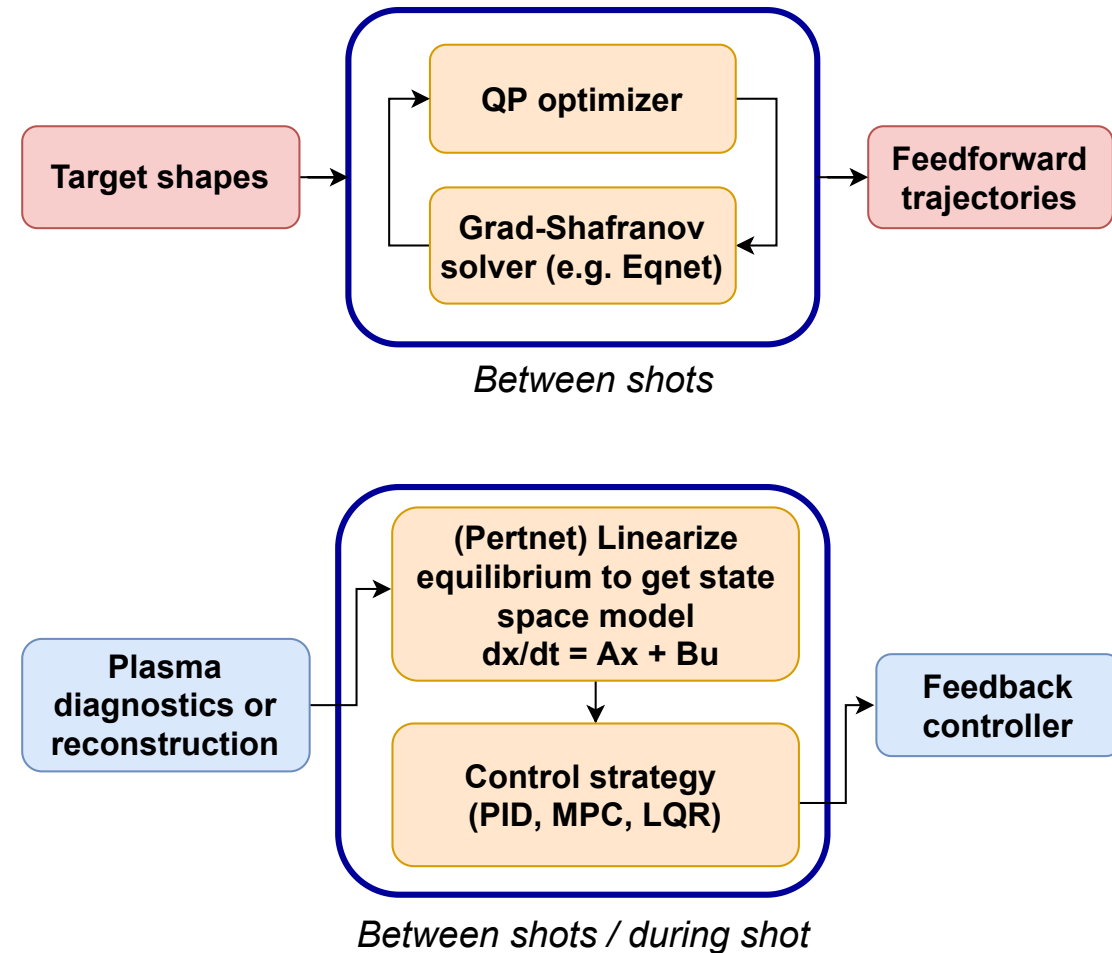


Neural net prediction of shaping parameters.

# NSTX-U feedforward shape control

# Motivation: upgrade NSTX-U shape control to include feedforward

- NSTX-U isoflux shape control algorithm relies entirely on feedback, which caused some difficulties during previous campaign.
  - Oscillations and tracking errors
  - Shot-to-shot tuning of PID gains
- Control could be improved by using feedback to adjust target coil currents around a reference current trajectory
- Optimizer can also be used to plan around constraints, minimize OH usage and extend shot, etc.
- Neural nets developed for *fast* implementations



# Feedforward shape design algorithm

## Step 1: user inputs

### Targets:

- boundary  $(R_b, Z_b)(t)$
- touch or x-point  $(R_{bdef}, Z_{bdef})(t)$
- plasma current  $I_p(t)$

### Initial currents $(I_c, I_v, I_p)(t=t_0)$

Non-inductive current  $I_{p,NI}$

### Parameters for (step 2) estimating plasma resistance

$R_p(t)$  and plasma flux  $\psi_{pla}(t)$ .

- for example:  $R_p(t)$ ,  $W_{mhd}(t)$ ,  $I_i(t)$

## Step 2: estimate plasma properties ( $R_p$ , $\psi_{pla}$ )

### Estimate $R_p(t)$ :

- direct user input of  $R_p$  or  $T_e$
- multishot average of resistivity  $\eta(t)$  (==current method)
- transport modeling with actuators (not implemented)

### Estimate the plasma $\psi_{pla}(t)$ :

- Several methods implemented that trade off speed, accuracy, and flexibility. For details see appendix.

A. custom semi-fixed boundary solver

B. gsdesign

C. eqnet

# Feedforward shape design algorithm

## Step 3: formulate and solve optimization for coil currents

- The shape control model uses a circuit equation for the coil, vessel, and plasma current dynamics. This can be rearranged into state-space form.
  - $v$  = voltages,  $R$  = resistance,  $I$  = currents,  $M$  = mutual inductance,  $\psi$  = flux

$$v_i = R_i I_i + \sum_j \left( M_{ij} \dot{I}_j + \frac{\partial \psi_{i,plasma}}{\partial I_j} \dot{I}_j \right)$$

$$\begin{aligned} \dot{\mathbf{I}} &= \mathbf{A}(t)\mathbf{I} + \mathbf{B}(t)\mathbf{v} \\ \mathbf{A}(t) &:= -(\mathbf{M} + \mathbf{X}(t))^{-1}\mathbf{R} \\ \mathbf{B}(t) &:= (\mathbf{M} + \mathbf{X}(t))^{-1} \end{aligned}$$

$$\mathbf{X}_{ij} := \frac{\partial \psi_{i,plasma}}{\partial I_j}$$

- Define our outputs  $y$  as the currents and isoflux shape errors.

$$x := [I_v \ I_p], \quad u := I_c$$
$$y = y_e + \delta y$$
$$y = \begin{bmatrix} I_c \\ I_v \\ I_p \\ \psi|_{R_b, Z_b} - \psi|_{R_{bdef}, Z_{bdef}} \\ \nabla \psi|_{R_{bdef}, Z_{bdef}} \end{bmatrix}$$

- Optimize a constrained quadratic cost function of the outputs  $y$  versus targets  $r$ . Outputs at future times are predicted via the dynamics model.

$$x_{k+1} = Ax_k + Bu_k$$

$$\delta y_k = C\delta x_k + D\delta u_k$$

$$\text{minimize } J = \sum_{k=1}^N (y_k - r_k)^T Q (y_k - r_k) + \Delta y_k^T Q_v \Delta y_k$$

## Step 4: Iterate

- In plasma estimation step (step2), solutions implicitly depend on the total flux/applied flux/coil currents.
- If we have reasonable knowledge of plasma parameters(t), then don't need to iterate.
- However, if estimates are not known then iteration likely needed. For example, if we explicitly evolve profile dynamics (not yet implemented) then need to account for coil current trajectories as profile actuators.
- Example: can use Li as a fitting parameter in estimating  $\psi_{pla}$ , but also depends on OH/ $I_p$  ramp rate.



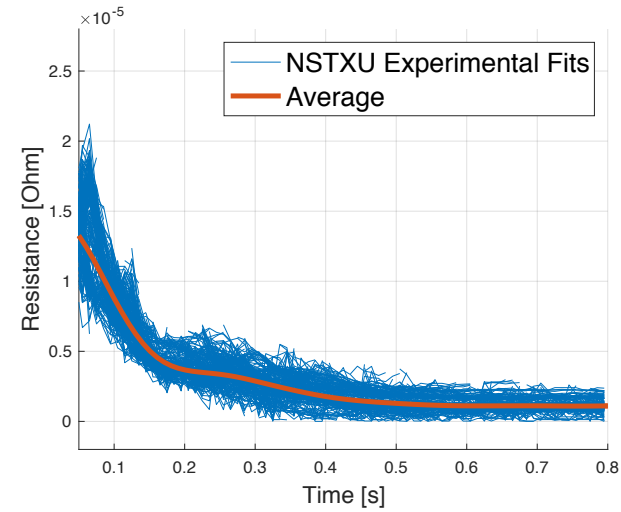
# Example: recreate NSTX-U 204660

## User inputs

- Target boundary and  $I_p$  obtained from experimental EFIT01 equilibria
- $I_p$ ,  $W_{\text{MHD}}$ , and boundary given as inputs to semi-fixed boundary solver for step 2

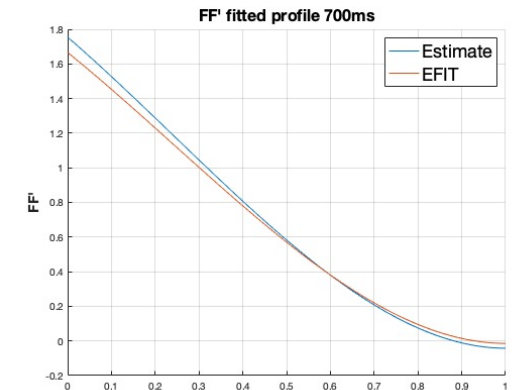
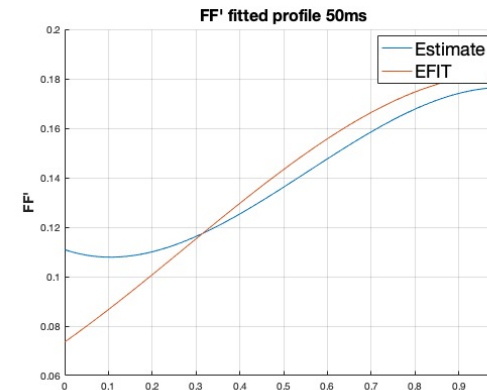
## Estimate $R_p$ and $\psi_{\text{pla}}$

- $R_p$ : plasma resistance is estimated as average resistance from campaign.
- $\psi_{\text{pla}}$ : semi-fixed boundary solver is a simple & fast implementation that scales averaged EFIT01 FF' and P' profiles to match  $I_p$  and  $W_{\text{MHD}}$ .
- (This can be a gross approximation, but optimizer is fairly robust to internal profile details.)



$$R_p = 1/I_p (V_{loop} - L_p \dot{I}_p)$$

Fig 1: plasma resistances fits from 2015-16 campaign



Figs 2 and 3: Examples of FF' fitting approximations found by solver. Optimizer is robust against this level of approximation.

# Example: recreate NSTX-U 204660

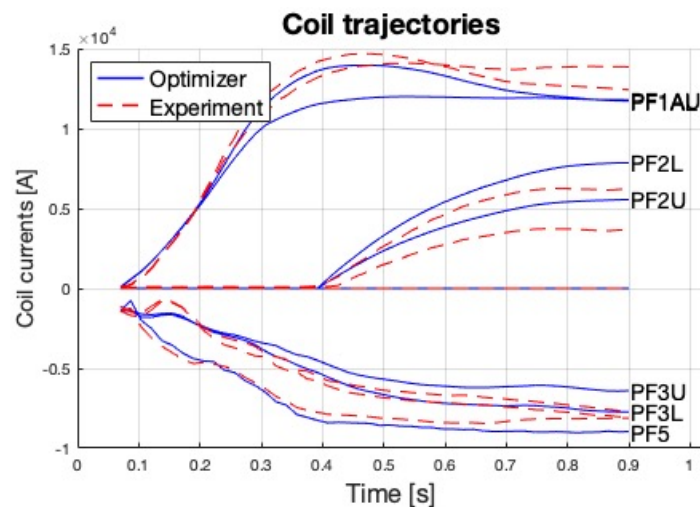


Fig 1A: coil currents, PF2 unconstrained

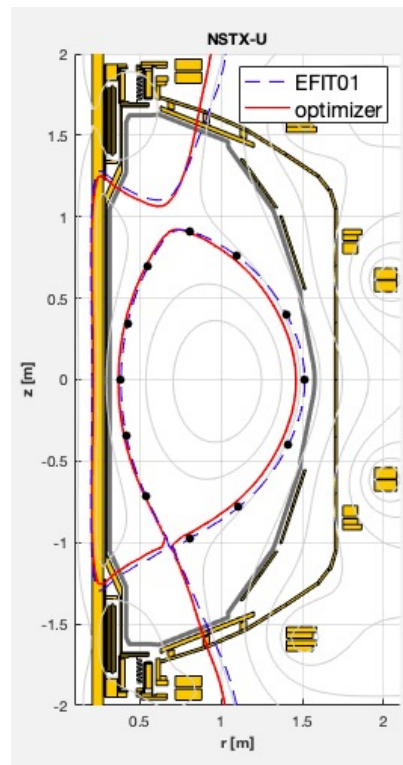


Fig 2A: Equilibrium at final time, PF2 unconstrained

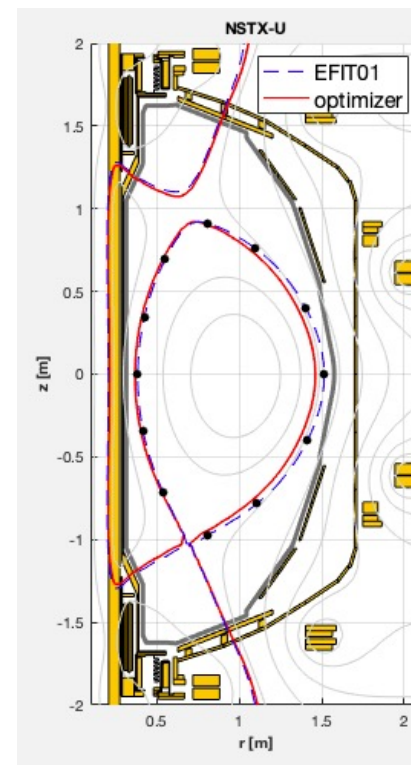


Fig 2B: Equilibrium at final time, PF2 constrained

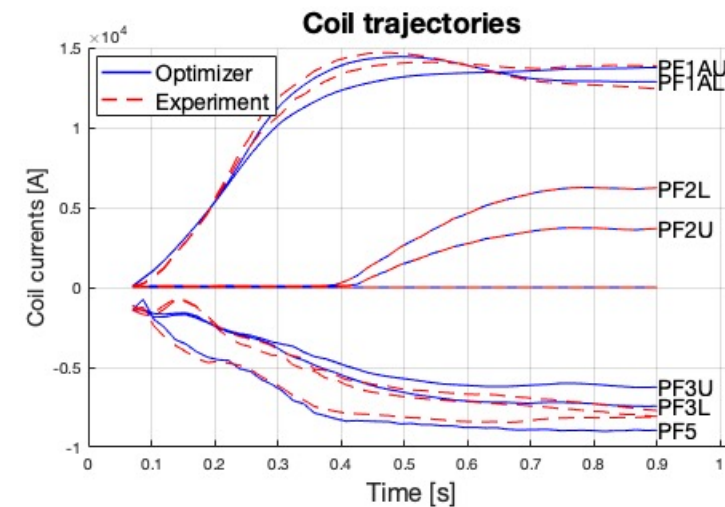


Fig 1B: coil currents, PF2 constrained

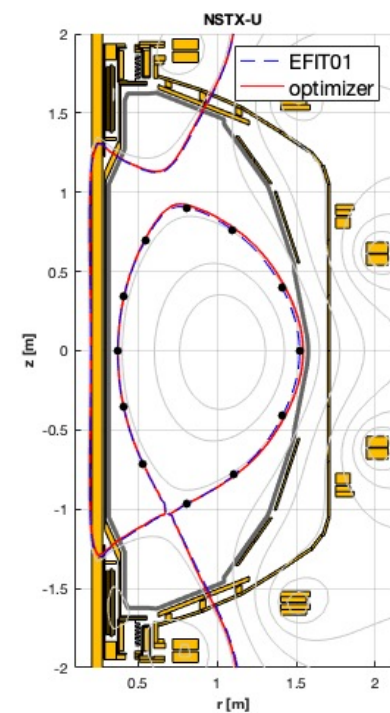
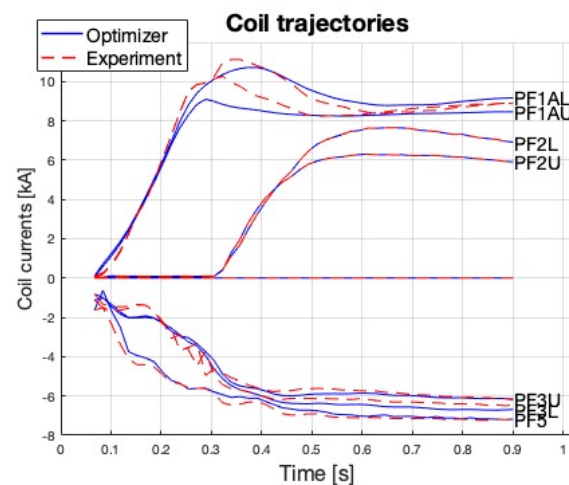
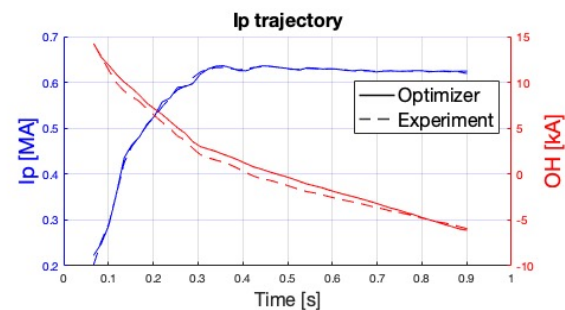
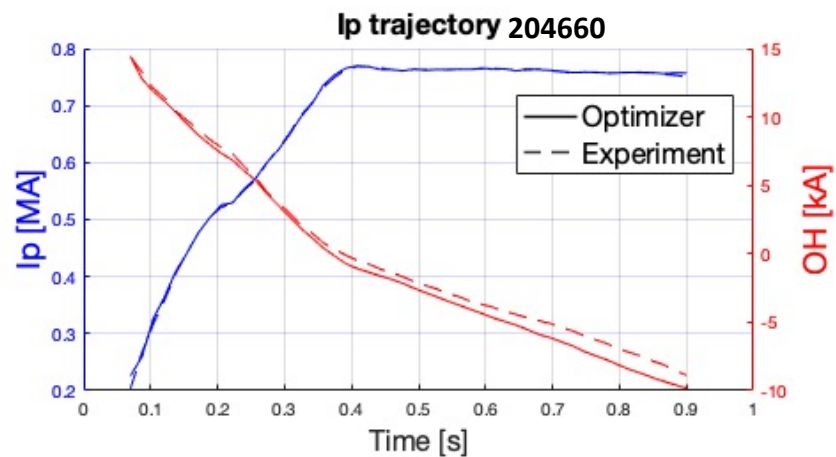
- Optimizer initially finds a different set of coil currents (**Fig 1A**) than was obtained in experiment. This can be interpreted as a “lower cost” solution to the shape optimization.
- If PF2U/L are constrained to experimental values, other coils converge towards experiment (**Fig 1B**)

Both optimization examples have similar shape errors, which are attributed to the  $\psi_{\text{pla}}$  estimate. (If exact FF'/P' profiles are given, shape error  $\rightarrow$  0.0cm)

# Example: recreate NSTX-U 204660 / 204069

- $I_p$ /OH match with experiment well, but some deviation due to  $R_p$  approximation (good enough for feedforward).
- Relationship is sensitive to  $R_p$ , and in practice would be improved by more detailed modeling or reference shots. However, shaping is not overly sensitive to OH.

Another example:  $I_p$ , coil trajectories, and final shape for 204069:



# Feedforward shape designs: next steps

## Next steps:

- quantify sensitivity of feedforward solutions to assumptions
- Test the combined feedforward + feedback system with gsevolve [Welander, 2019] simulations. How accurate does the feedforward need to be?

## General thoughts:

- System takes input profiles and optimizes coil trajectories and flux maps, i.e. it decouples the profile optimization from shape optimization.
- On first principles this may not seem like a good idea, but results look promising for NSTX-U. There is a practical advantage since it is difficult to solve both optimizations simultaneously
  - Profile optimizers often use prescribed shapes ([Felici, 2012], [Teplukhina, 2017])
  - Most self-consistent coupled simulators not designed for optimization

# Neural net equilibrium and dynamics modelling

# Neural nets for shape control

- **Eqnet:**

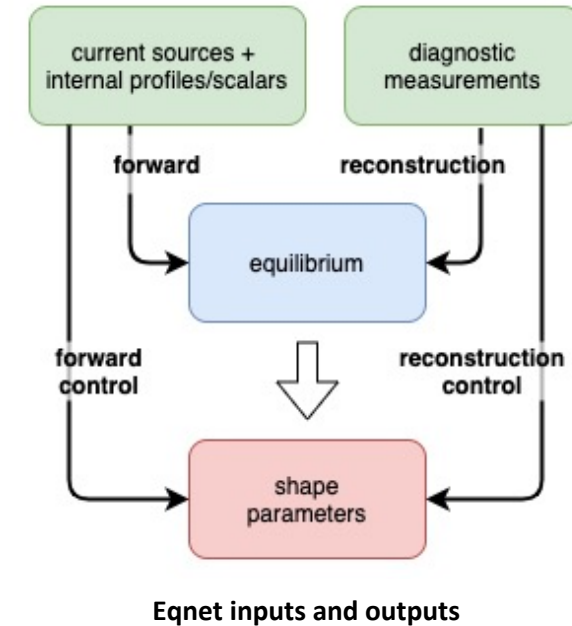
- neural net equilibrium solver
- several modes of operation. Predict flux surfaces or shaping parameters from diagnostics or profiles.
- Useful for, e.g., estimating  $\Psi_{\text{pla}}$  for the shape optimizer.

- **Pertnet:**

- predicts the non-rigid plasma response  $\frac{\partial \psi_{\text{plasma}}}{\partial I}$  which is a nonlinear term in the shape control model (how the plasma redistributes in response to coil current perturbation)
- trained on gspert code outputs [Welander, 2005]

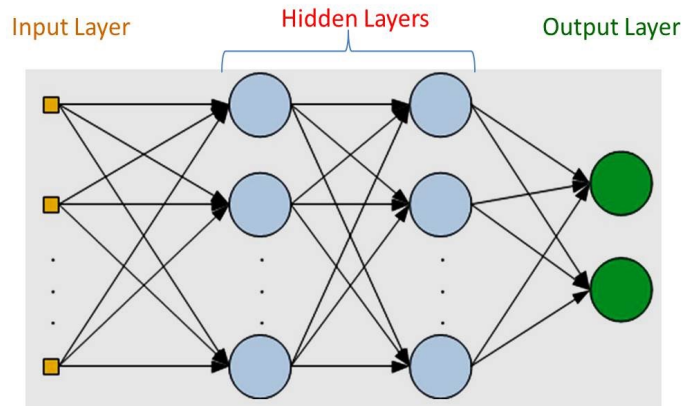
$$v_i = R_i I_i + \sum_j \left( M_{ij} \dot{I}_j + \frac{\partial \psi_{i,\text{plasma}}}{\partial I_j} \dot{I}_j \right)$$

$$\begin{aligned} \dot{x} &= A(t)x(t) + B(t)u(t) \\ y(t) &= C(t)x(t) + D(t)u(t) \end{aligned}$$

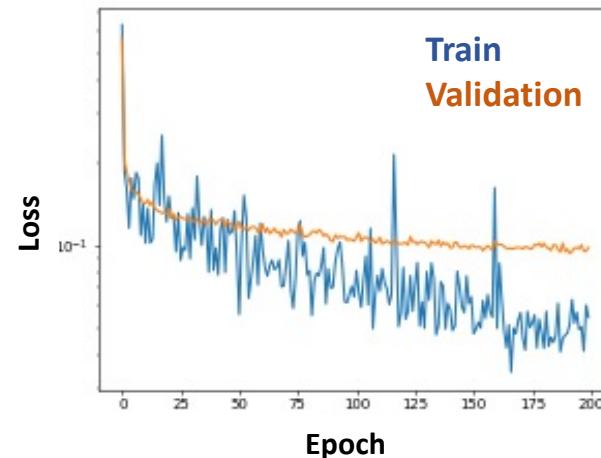


# Neural net architectures

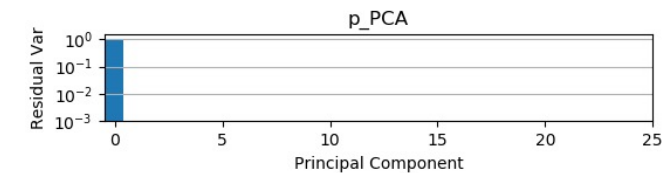
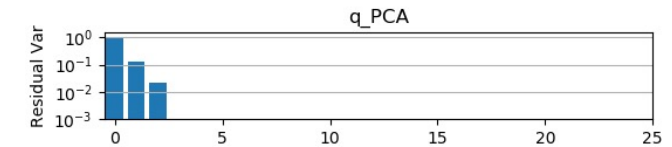
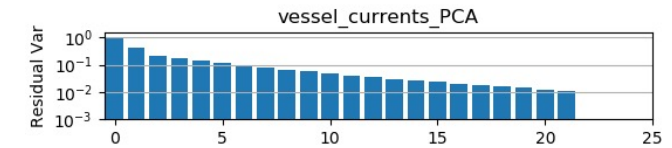
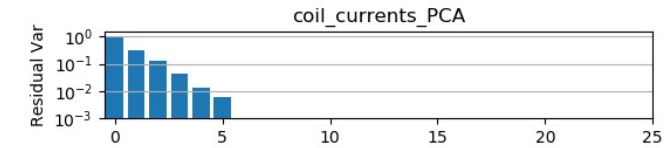
- Both NNs use multilayer perceptron (MLP) architectures with PCA reduction of inputs and outputs to capture 99.9% variance.
- Train, validation, test split is 80-10-10 by shot number
- Trained in PyTorch using a gridscan for hyperparameters
  - Eqnet: 6 hidden layers, size 800, ELU activation, no dropout
  - Pertnet: 3 hidden layers, size 200, ReLU activation, 10% dropout



Multilayer perceptron



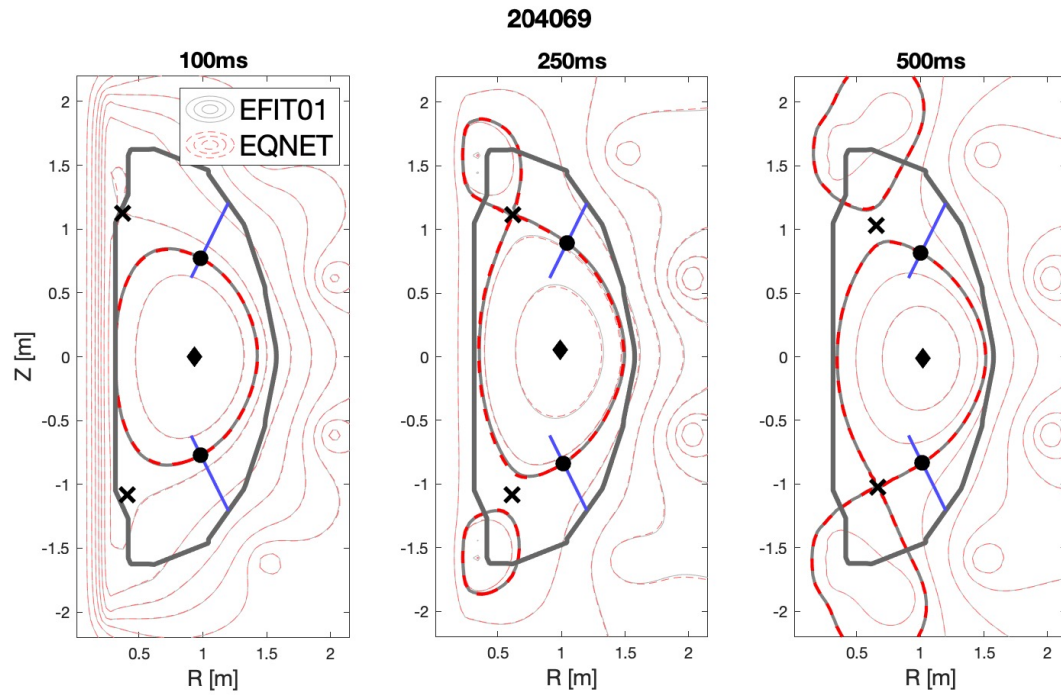
Training loss curve



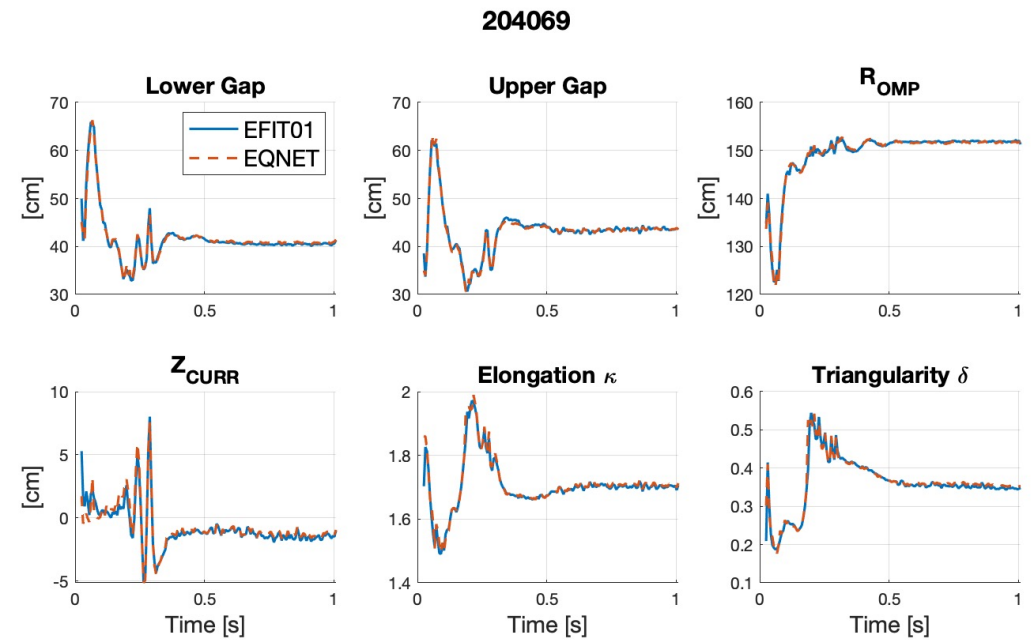
PCA components for a subset of the input variables

# Eqnet results

- Eqnet results (from validation dataset)



Equilibrium flux predictions capture range of equilibria (limited, USN, LSN)

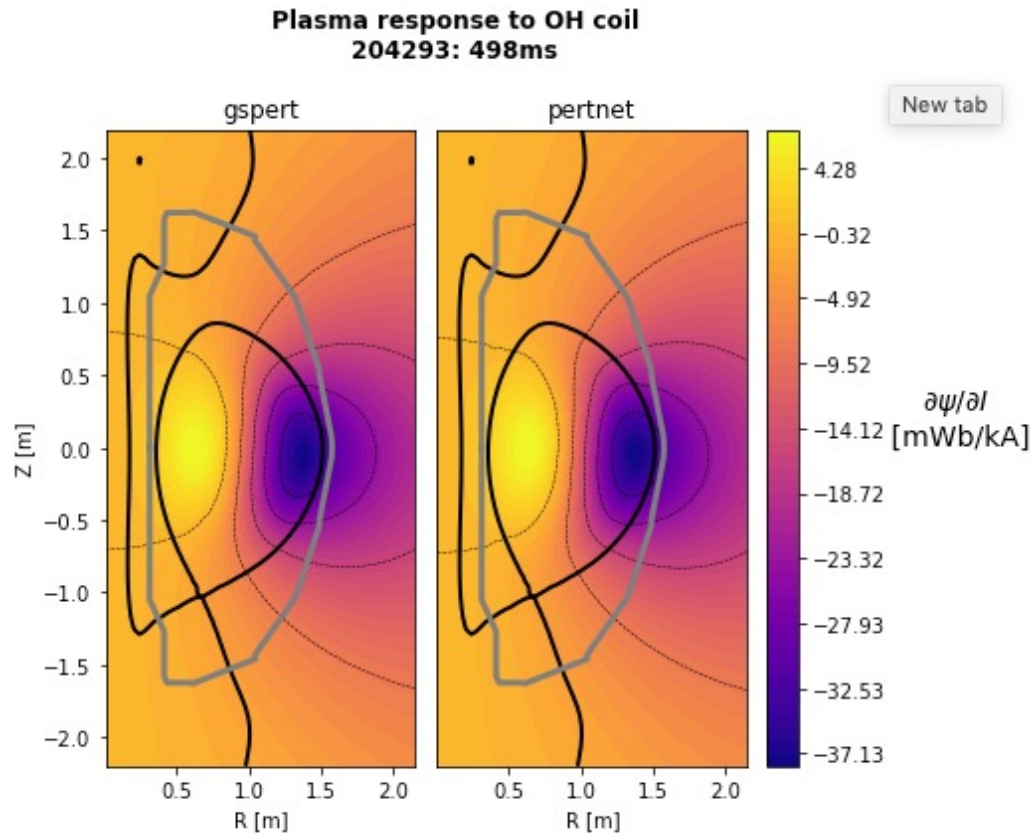


Good prediction of shaping parameters



# Pertnet results

- Pertnet results (from validation dataset)

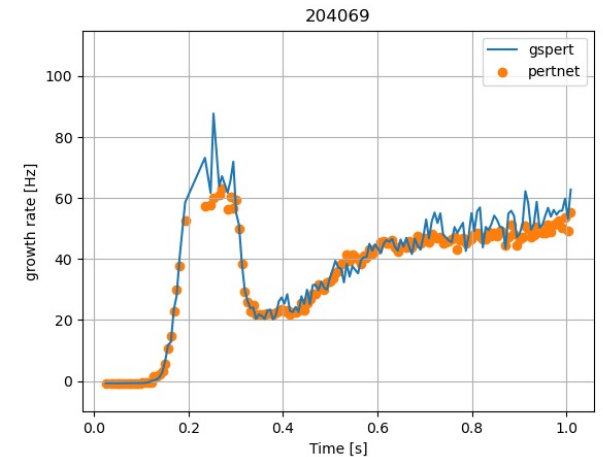
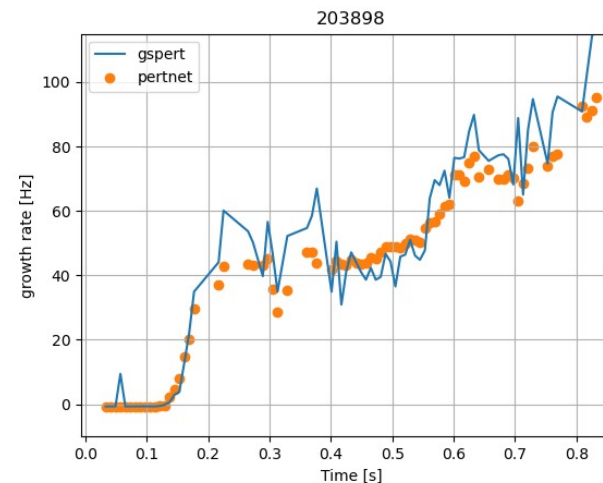


- Growth rate ( $\gamma$ ) can be obtained from flux responses
- Flux responses give good estimates of growth rate, even though NN not trained to estimate growth rate directly.

$$X_{cc} = M_{cp} M_{pp}^{-1} \frac{\partial \psi_p}{\partial I_c}$$

$$A = -(M_{cc} + X_{cc})^{-1} R_c$$

$$\gamma = \max \text{eigenvalue}(A)$$



# Conclusion

# Conclusions

- Design tool created for optimizing feedforward currents on NSTX-U in order to match desired shape targets.
- Shows good agreement with previous experimental data and can be used to design optimize/design combined feedforward + feedback control algorithms.
- Equilibrium and perturbation neural nets also developed to speed up compute-intense portions of code and implementation is in-progress.

# References

- A. Welander *et al* 2005 *Fusion Science and Technology*, **47** 763-767
- A. Welander *et al* 2019 *Fusion Engineering & Design* **146** 2361-2365
- F. Felici and O. Sauter 2012 *Plasma Phys. Control. Fusion* **54** 025002
- A.A. Teplukhina *et al* 2017 *Plasma Phys. Control. Fusion* 59 124004

## **Acknowledgements:**

- This work supported by DOE contract DE-SC0015878 and DE-AC02-09CH11466.

# Appendix

# Feedforward shape design algorithm: step 2 details

## Step 2: estimate plasma flux distribution $\psi_{\text{pla}}$

### A. custom semi free-boundary solver

$I_p, W_{\text{mhd}}, (R_b, Z_b), \text{EFIT01 average profiles } P_0', FF_0' \rightarrow \psi_{\text{pla}}$

Scales  $P_0', FF_0'$  in order to match  $I_p, W_{\text{mhd}}$   
~2 iterations is OK

+ fast, reasonably accurate

- need  $W_{\text{mhd}}$  a-priori, profile assumption weak

### B. gsdesign

Flexible inputs (e.g.,  $I_p, \text{betap}, li, \text{boundary}$ )  $\rightarrow \psi_{\text{pla}}$

+ well-established tool, flexibility in inputs, generalizability, accuracy

- speed, profiles (so far, have not been able to figure out some desired behavior for profiles like shift/scale a given  $FF'$ . Can shift/scale a linear  $FF'$ , or match a target profile).

### C. Eqnet neural network

Flexible inputs (e.g.,  $I_p, \text{betap}, li, \text{boundary}$ )  $\rightarrow \psi_{\text{pla}}$

Have not yet trained for this particular mode of operation, but accurate for similar problems

+ speed, accuracy(?)

- accuracy(?), generalizability, flexibility